

AD-A043 786

TEXAS UNIV AT EL PASO DEPT OF ELECTRICAL ENGINEERING  
THE ATMOSPHERIC SCIENCES LABORATORY PHOTODISSOCIATION-RADIATION--ETC(U)  
JUL 77 J L COLLINS

F/G 9/2

DAAD07-74-0263

UNCLASSIFIED

ECOM-77-4

NL

| OF |  
AD  
A043 786



END  
DATE  
FILMED  
9-77  
DDC



8

AD

Reports Control Symbol  
OSD-1366

RESEARCH AND DEVELOPMENT TECHNICAL REPORT  
ECOM-77-4

AD A 043786

# THE ATMOSPHERIC SCIENCES LABORATORY PHOTODISSOCIATION- RADIATION MODEL OF THE MIDDLE ATMOSPHERE

## A USERS MANUAL

By

**Jerry Collins**

**Electrical Engineering Department**

The University of Texas at El Paso

El Paso, Texas 79968

**Contract Monitor: Harold N. Ballard**

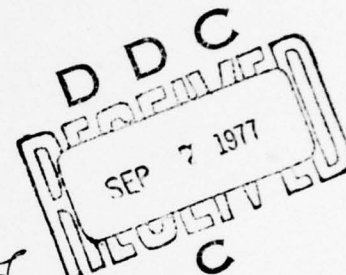
**Atmospheric Sciences Laboratory**

US Army Electronics Command

White Sands Missile Range, New Mexico 88002

**July 1977**

Approved for public release; distribution unlimited.



DDC FILE COPY

# ECOM

UNITED STATES ARMY ELECTRONICS COMMAND - FORT MONMOUTH, NEW JERSEY 07703

## **NOTICES**

### **Disclaimers**

The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

The citation of trade names and names of manufacturers in this report is not to be construed as official Government indorsement or approval of commercial products or services referenced herein.

### **Disposition**

Destroy this report when it is no longer needed. Do not return it to the originator.

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER ECON-77-4	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
4. TITLE (and Subtitle) THE ATMOSPHERIC SCIENCES LABORATORY PHOTODIS- SOCIATION-RADIATION MODEL OF THE MIDDLE ATMOSPHERE - A USERS MANUAL		5. TYPE OF REPORT & PERIOD COVERED SPECIAL REPORT. no. 11	
7. AUTHOR(s) Jerry L. Collins		6. PERFORMING ORG. REPORT NUMBER #11	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Electrical Engineering Department University of Texas at El Paso El Paso, Texas 79968		8. CONTRACT OR GRANT NUMBER(s) DAAD07-74-C-0263	
11. CONTROLLING OFFICE NAME AND ADDRESS United States Army Electronics Command Atmospheric Sciences Laboratory White Sands Missile Range, New Mexico 88002		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) United States Army Electronics Command Atmospheric Sciences Laboratory White Sands Missile Range, New Mexico 88002		12. REPORT DATE July 1977	
		13. NUMBER OF PAGES 47	
		15. SECURITY CLASS. (of this report) UNCLASSIFIED	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES Contract Monitor: Mr. Harold Ballard Atmospheric Sciences Laboratory White Sands Missile Range, NM 88002			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A computer code to calculate time- and altitude-dependent photodissociation rates and transmitted solar flux intensities in the upper atmosphere has been developed, for Atmospheric Sciences Laboratory, and is operational on the UNIVAC 1108 computer system, at White Sands Missile Range. This document is presented to demonstrate to the interested user how to set up and execute the program. Included is a brief discussion of the files of absorption coefficients stored in FASTRAND direct access files and the various solar flux			

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

408579



SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

tape files which are stored in the UNIVAC 1108 System B Library.

Sixteen internally documented auxiliary programs available for plotting, file management, etc., are briefly described in Appendix A.

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

# TABLE OF CONTENTS

	Page
1. INTRODUCTION . . . . .	1
2. PROGRAM INPUT . . . . .	2
3. EXECUTION SET-UP . . . . .	10
4. LOGICAL FLOW . . . . .	12
5. MATHEMATICAL CALCULATIONS . . . . .	13
6. SAMPLE OF INPUT . . . . .	15
7. SAMPLE OF OUTPUT . . . . .	21
REFERENCES . . . . .	45
APPENDIX A: AUXILIARY PROGRAMS AND FILES . . . . .	46

ACCESSION for	
NTIS	White Section <input checked="" type="checkbox"/>
DDC	B ft Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
DISSEMINATION	
BY	
DISTRIBUTION/AVAILABILITY NOTES	
SPECIAL	
A	

## 1. INTRODUCTION

The JVALUE program was developed to calculate photodissociation rates as a function of time, geographical location and altitude and is part of ANMAR, the ASL Numerical Model of Atmospheric Radiation, Composition and Dynamics. The photodissociation rates are used as input data for ASA, the chemical kinetic modeling program, also part of ANMAR. Altitude and time dependent solar flux intensities are predicted also. The computational technique has been reported previously.<sup>1,2</sup>

The software package is comprised of a single FORTRAN program to compute instantaneous rates. Because of the way in which ASA utilizes the photodissociation rates, only the noon, or maximum values need be calculated. If mean rates, averaged over several solar zenith angles are desired, a second FORTRAN program, MEAN, is available for the averaging. MEAN, and several other internally documented auxiliary programs, are listed and their respective functions briefly described in Appendix A.

Logical parameters within the program allow the selection of card, tape or FASTRAND output for the photodissociation rates. Solar flux intensities are stored on magnetic tape.

Card input to the program includes program control parameters, latitude and time for the calculation of solar zenith angles, wavelength intervals, quantum efficiencies, identification of the specific photodissociation processes considered, and density profiles for the set of absorbers. Experimental profiles are used when available, and other densities are predicted by ASA. In addition to the card input, a direct access file containing the absorption coefficients and the solar flux data must be supplied. All input data is described in more detail in the following sections.

2. PROGRAM INPUT  
A. CARD INPUT

Card Type 1

COL.	NAME	FORMAT	DESCRIPTION
2-5	\$NLV	Unformatted	Defines namelist to follow.
6-n	JAYS		If JAYS = <code>·FALSE·</code> , the subroutine to sum the individual photodissociation rates will not be called.
	PCH		If PCH = <code>·TRUE·</code> , rates will be punched on cards in ASA format.
	ITAPE		If ITAPE = <code>·TRUE·</code> , rates will be written on Unit 9 (tape or FASTRAND) in ASA format for storage, plotting, etc.
	IPHI		If IPHI = <code>·TRUE·</code> , NSPEC factors will be read in to modify SIGMA, the total absorption coefficient, and SSIGMA, the photodissociation coefficient, or to modify the density profiles.
	DEN		If DEN = <code>·TRUE·</code> , the input density profiles will be written out for each absorber.
	DATA		If DATA = <code>·TRUE·</code> , input solar flux and absorption data will be written out. This should be invoked only for debugging or the examination of a small absorbing interval because more than 600,000 values, many of them zero, could be written out.
	SSUMIT		If SSUMIT = <code>·TRUE·</code> , program will sum photoabsorption rates (from output FASTRAND file 8) only. This option prevents loss of the calculated values in case of machine error. It may also be used to examine the contribution from various absorbing intervals for a given specie.



## Card Type 1 (contd.)

COL.	NAME	FORMAT	DESCRIPTION
	NFIL		The size of the input direct access file of absorption coefficients must be supplied. This value must be at least as large as IVAL2, the final wavelength.

last5

Columns V\$END

Terminates namelist.

Note: All logical parameters are set to false in the program with the exception of JAYS, which is true. The namelist card is used to invoke the other options when desired and to furnish NFIL.

## Card Type 2

1-5	MON	15	Month of year,
6-10	MDAY	15	day of month,
11-15	NHOUR	15	time in hours
16-20	MIN	15	and minutes (MST), for which photo-dissociation rates are to be calculated.
21-25	INC	15	Time increment in minutes if more than one zenith angle is to be calculated.

## Card Type 3

1-15	(LA(I), I=1,3)	3I5	Latitude in degrees, minutes and seconds.
1-15	(LN(I) I=1,3)	3I5	Longitude in degrees, minutes and seconds.

## Card Type 4

1-72	(TITLE(I), I=1,12)	12A6	Alphanumeric identification of the run.
------	-----------------------	------	---



## Card Type 5

COL.	NAME	FORMAT	DESCRIPTION
1-5	IVAL1	I5	First
6-10	IVAL2	I5	and last wavelength to be considered in the calculation
11-15	MSPEC	I5	The number of attenuating species. If all of the chemical absorbers are to be used to calculate the amount of solar flux transmitted, MSPEC = NSPEC, the number for which photodissociation rates are to be calculated.
16-20	NPOS1	I5	Number of solar flux values to skip so that the input tape will be positioned at IVAL1.
21-25	NPOS2*	I5	Key to control printed output. = 0 writes out only final output -- the rates as a function of altitude plus the card, FASTRAND, and/or tape output as specified. = 1 writes out all computed flux values. < 0 writes out all individual contributions to the photodissociation rates. > 1 writes out all of the above.
26-30	ISKIP	I5	Number of layers for which photodissociation rates will not be calculated.

\*Note: This is primarily for debugging since writing out all data in a normal sized run would take many hundreds of pages. To examine the calculated solar flux values, the SOLPLT or the RADPLT program would be preferable. Examination of the per-interval contribution to photodissociation rates is better handled through input data to subroutine SUMIT and the logical option SSUMIT.

## Card Type 6

1-5	NSPEC	I5	Total number of species which photodissociate.
6-10	NTHETA	I5	Up to twelve solar zenith angles may be computed but due to the very large

## Card Type 6 (cont'd.)

COL.	NAME	FORMAT	DESCRIPTION
			output file 8 required (about 400 tracks/zenith angle), only one angle at a time is recommended.
11-15	NTOP	I5	Highest altitude to calculate (km).
16-20	NLAYER	I5	Number of altitudes to calculate (including NTOP).
21-25	NWAVE	I5	NWAVE = 100, the maximum number of wavelengths per cycle, where NCYCLE = (IVAL2-IVAL1)/100. Due to storage requirements, the computation is divided into NCYCLE intervals.
26-35	DZ	E15.5	The depth of each model layer in cm, currently set to $5 \times 10^7$ cm (5km).

## Card Type 7

1-42	(LAYER(I), I=1,14)	14I3	NLAYER altitudes to calculate.
------	-----------------------	------	--------------------------------

## Card Type 8

1-10	SYMB	A6,4x	Chemical symbol for absorber (right-justified).
11-40	(N(K,J), J=1,6)	6I5	<p>Wavelengths which define the thresholds for up to five photodissociation processes for the Kth specie (of NSPEC species). N(K,1) will always be set to IVAL1, the initial wavelength. For example, the 4th absorber in one set of coefficients is NO<sub>2</sub>. N(4,2) - N(4,1) defines the wavelength interval for the reaction</p> $\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}(^1\text{D})$ <p>and N(4,3) - N(4,2) + 1 defines</p> $\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}.$

Note: There are NSPEC cards of type 8.

## Card Type 9

COL.	NAME	FORMAT	DESCRIPTION
1-5	NEQ	I5	Total number of photodissociation reaction rates to be calculated.

## Card Type 10

1-5	NS(I)	I5	Ith photodissociation process for a specie. (See note on Card Type 7.)
6-10	NE(I)	I5	NE(I) is the number of the chemical reaction in ASA which corresponds to the NS(Ith) photodissociation rate.
11-15	NR(I)	I5	The number of the specie in the set of chemical absorbers (contained in the direct access file).
16-20	FACTOR(I)	F5.3	Quantum efficiency.
20-66	(EON(I,J), J=1,6)	6A6	The alphanumeric representation of the chemical reaction and absorbing interval for identification purposes.

Note: There are NSPEC cards of type 10. To clarify this type card, an example is given:

3 1 11.000 0<sub>2</sub> + hv → O + O 1759-2500 Å

Field 1 specifies that this is the third photodissociation process for molecular oxygen, field 2 shows that it is reaction 1 in the current chemical kinetic scheme, and field 3 shows that oxygen is the first absorber in the set of absorption data. Field 4 shows a quantum yield of 1.000, and the balance of the card identifies the photodissociation reaction.

## Card Type 11

1-12	EN(J,L)	E12.6	The average number density of the Jth specie at the center of the Lth layer.
13-24	SYMB(J)	6x,A6	The chemical symbol of the Jth specie.
25-34	LAYER(L)	6x,I3	The altitude of the Lth interval.

## Card Type 11 (contd.)

COL	NAME	FORMAT	DESCRIPTION
-----	------	--------	-------------

Note: There are NLAYER cards for each of the NSPEC chemical species. The first card for each specie is the column density above the model.

## Card Type 12

1-5	PHII (I)	F5.2	If IPHI = .TRUE., constant factors may be read in to adjust the entire set of total and photodissociation coefficients for each chemical absorber in the set. These constant factors also may be used to adjust the density profiles for given absorbers.
6-10	PHI (I)	F5.2	
.			
.			
.			

Note: PHII and PHI values for each of the NSPEC absorbers are contained on consecutive cards, eight sets to each card.

Since there is so much card input, most or all of this data is usually stored in an ELT element within the program file. This data may then be referenced with the ADD Furpur. A sample of input data is given in Section 6.

## B. INPUT DATA FILES

- (1) An input tape of solar flux values must be supplied to the program. The following sets are available in the UNIVAC 1108 Computer B Tape Library:

File 1	Brinkman-Thakaeakara <sup>3,4</sup> composite data	26-7500 Å
File 2	Ackerman <sup>5</sup>	1176-7275 Å
File 3	File 1 with Broadfoot <sup>6</sup> data used in the 2000-3100 Å interval	26-7500 Å

These solar flux values have been averaged in units of photons-  
cm<sup>-2</sup> sec<sup>-1</sup> Å<sup>-1</sup> in 5(F10.2,E15.5) format.

- (2) The direct access file of absorption coefficients, referenced internally as KFILE, contains data averaged over 1 Å intervals for up to 18 absorbers. The file-handling sub-routines, LOADUA and DACCESS, deliver NCYCLE sets of NWAVER



(100) total and dissociation absorption coefficients for each of the NSPEC species. The following relationships exist between the absorption coefficients and the cross-sections:

$$k_{i_T}(\lambda) = n_o \sigma_{i_T}(\lambda),$$

$$k_{i_D}(\lambda) = n_o \sigma_{i_D}(\lambda),$$

and

$$\sigma_{i_D}(\lambda) = \phi_i(\lambda) \sigma_{i_T}(\lambda).$$

where

$\sigma_{i_T}(\lambda)$  = Total absorption cross-section for the  $i$ th specie ( $\text{cm}^2$ ).

$k_{i_T}(\lambda)$  = Total absorption coefficient for the  $i$ th specie ( $\text{cm}^{-1}$ ).

$k_{i_D}(\lambda)$  = Dissociation coefficient for the  $i$ th specie ( $\text{cm}^{-1}$ ).

$n_o$  = Loschmidt's number ( $\text{n-cm}^{-3}$ ).

$\phi_i(\lambda)$  = Quantum yield for a given photodissociation process of the  $i$ th specie.

$\sigma_{i_D}(\lambda)$  = The dissociation cross-section of the  $i$ th specie.

Very seldom are variable quantum yields known; therefore,  $\sigma_{i_T}(\lambda)$  and  $\sigma_{i_D}(\lambda)$  are set equal for most species. Constant quantum yields are best applied in subroutine SUMIT.

At present, data for fourteen absorbers are contained in one 270 track direct access file, COLLINS\*COEFF. A second file, COLLINS\*COEFF1., contains alternate data for several species. Additional data for eleven species not considered in ASA are stored in COLLINS\*COEFF2. Initially, an extensive literature search<sup>1</sup> was made for absorption data and all data were generated over 1 Å averages using an interpolation program (COLLINS\*JONE3). Generated and original data sets were plotted to ascertain if corrections were required to maintain the integrity of the



maxima and minima. Usually sets of two- and four-point interpolations of the data were blended with original data to give a "best set." Where two or more sets of data were combined, it was often necessary to smooth data at the position of overlap. Backup tapes of these "best sets" are stored in the UNIVAC 1108 Computer B Tape Library with alternate sets stored for some species - primarily molecular oxygen, ozone, nitrogen dioxide and nitrous oxide.

These data also are stored in a (36 x N) array in the FASTRAND direct access file, with N set by the number of tracks chosen when the file is created. The program delivers (NSPEC x 100) values of the total and photodissociation coefficients from the direct access file to the main subroutine for (IVAL2-IVAL1) cycles for each layer calculated. Identifying wavelengths are also provided. (This file is more completely described in the internal documentation of Program DA.) All of the various data stored on mass storage in the UNIVAC 1108 system and Tape Library have been tabulated and identified in a notebook which is under the control of Harold Ballard, Contract Monitor.

## 3. EXECUTION SET-UP (EXEC-8 CONTROL CARDS)

Program execution requires the following sequence of control cards:

@QUAL	COLLINS	
@ASG,T	1.,T, (tape id)	The tape id is the UNIVAC Computer B Library number. This tape will be released after the first layer unless multiple zenith angles are computed.
@MSG,W BK101U PAN 8150 (user id)		The W option on the MSG card signals the computer operator to label the BK library tape with the label the user desires as identification.
@ASG,T	3.,T,BK101U	Output tape for solar flux data.
@ASG,T	7.,F,SCRTCH	Temporary storage for intermediate solar flux values.
@DELETE,C	*JAY.	File to store individual
@ASG,UP	*JAY.,F2/O/TRK/400	contributions to the photodissociation rates.
@USE 8.,*JAY.		
@DELETE,C	*12SEP.	File to store photodissociation
@ASG,UP	*12SEP.,F	rates. Required if
@USE 9.,*12SEP.		ITAPE=.TRUE.
@ENABLE,C	*COEFF.	This assigns the direct
@ASG,A	*COEFF.	access file containing
@USE KFILE.,*COEFF.		the absorption coefficients.
@ENABLE,C	*JVALUE.	
@ASG,A	*JVALUE.	
@XQT	*JVALUE.	
Input cards types 1-11		
@FIN		

Note: File 8 may be assigned as a temporary file; however, if there is difficulty with the machine when the program is near completion, all data will be lost. This file should be deleted after the successful termination of a job unless the user plans to use the SSUMIT option to look at contributions over various intervals. The @ENABLE,C and @DELETE,C cards are added to allow one to use the rerun option in case the job is lost due to machine error.

When a data set for a given set of absorbers at a given latitude has been assembled, one may use the ELT processor to diminish the card input for each run.

@ELT,IS                    \*JVALUE.CDATA  
    Input cards types 5-11

Then to execute:

@XQT                    \*JVALUE.  
    Input data cards 1-4

@ADD,PE                    \*JVALUE.CDATA

A sample of the program output may be found in Section 7.

#### 4. LOGICAL FLOW

Subroutine MAIN initially reads the logical parameters which specify the amounts and types of input/output data and the required input/output tape and FASTRAND files. The other card input data then is read into storage.

Subroutine ZEN, called by MAIN, calculates the specified number of solar zenith angles for the time of year and latitude. At this time, subroutines LOADUA and DACCESS check the size and open the direct access file. A second call to these subroutines specifies the wavelengths to be delivered for each program cycle. (Due to the large amounts of solar flux and absorption data required, only 100 wavelengths are calculated in each cycle.)

The attenuation of the solar flux and the per-Angstrom contributions to the instantaneous photodissociation rates are calculated for each 100 wavelengths. The former values are stored on a temporary magnetic tape file until all wavelengths have been processed, at which time all solar flux values calculated for that altitude interval are dumped on a UNIVAC 1108 Library Tape file. This file is then repositioned and these data become input data for the next altitude interval. The per-Angstrom contributions to the rates are blocked into a FASTRAND file.

When all altitudes have been processed, subroutine SUMIT is called to sum the per-Angstrom contributions over the appropriate intervals for each photodissociation reaction considered for the set of absorbers. The quantum yield, if known, is usually applied here. The rates will be punched on cards and/or written on a FASTRAND or tape file.



## 5. MATHEMATICAL CALCULATIONS

The basic equation used for the calculation of photodissociation rates in the upper atmosphere is:

$$J_j(z,t) = \int_{\lambda_1}^{\lambda_2} \phi_i(\lambda) \sigma_{T_i}(\lambda) I_{T_\lambda}(z,t) d\lambda \quad (1)$$

where:

- $J_j(z,t)$  = Rate of the  $j$ th photodissociation process of the  $i$ th specie in the wavelength interval  $\lambda_1$  to  $\lambda_2$  ( $\text{sec}^{-1} \text{ molecule}^{-1}$ ),
- $i$  = index for the  $i$ th chemical absorber.
- $z$  = altitude (cm),
- $t$  = time of day, month and year,
- $\sigma_{T_i}(\lambda)$  = total microscopic cross section for photoabsorption by the  $i$ th specie ( $\text{cm}^2$ ),
- $\phi_i(\lambda)$  = quantum yield of the  $i$ th specie, defined as the ratio of the dissociation cross section,  $\sigma_{D_i}(\lambda)$  to the total cross section, and
- $I_{T_\lambda}(z,t)$  = total intensity of the radiation about the interval  $d\lambda$  incident on the top of the layer centered at altitude  $z$  ( $\text{photons cm}^{-2} \text{ sec}^{-1} \text{ 0.1 nm}^{-1}$ ).

The photodissociation rate for a given density profile is given by

$$R_j(z,t) = \int_{z_1}^{z_2} J_i(z,t) [n_i(z,t)] dz \quad (2)$$

where



$R_j(z,t)$  =  $j$ th photodissociation rate ( $\text{sec}^{-1}$ ) of the  $i$ th specie at altitude  $z$  and time  $t$ ,

$[n_i(z,t)]dz$  = the total number of molecules of the  $i$ th specie in the altitude interval from  $z_1$  to  $z_2$ .

The intensity of the direct radiation incident upon the top of the model is obtained from the Bouguer-Lambert law<sup>7</sup>:

$$I_{D\lambda}(z,t) = I_{\lambda}(\infty) \exp \left\{ - \int_{\infty}^z [\alpha(\lambda,z,t) + \beta(\lambda,z,t)] \sec \theta_z(t) dz \right\} \quad (3)$$

where

$I_{\lambda}(\infty)$  = monochromatic radiation about the interval  $d\lambda$  outside the earth's atmosphere. Subsequent model layers use the last calculated value of the solar flux, and

$\alpha(\lambda,z,t) = \sum_i \sigma_{T_i}(\lambda) [n_i(z,t)]$ , the attenuation coefficient due to absorption, ( $\text{cm}^{-1}$ ),

$\beta(\lambda,z,t) = \frac{32\pi^3 (\mu - 1)^2}{3 \sum_i [n_i(z,t)] \lambda^4}$ , the attenuation coefficient due to Rayleigh scattering ( $\text{cm}^{-1}$ ),<sup>8,9,10</sup>

$\mu$  = index of refraction of air,

$\lambda$  = wavelength (cm), and

$\sec \theta_z(t)$  = solar zenith angle at time  $t$  for a given geographic location, calculated by the standard approximation<sup>11</sup>.

The contribution due to scattering is based on the Leighton<sup>9,10</sup> approximation.

## 6. SAMPLE OF INPUT

Shown in this section is a complete set of the required cards needed to execute the computer code JVALUE.

SNL ITAPE=.TRUE.,NFIL=8500, DEN=.TRUE.,IPHI=.TRUE. SEND

9 28 12 0 0

16

32

106

SEPT 32 NORTH COMPOSITE 9/28/76

976 3975 4 950 0 0

16 1 70 5 100 0.50 E 06

75 70 65 60 55 50 45 40 35 30 25 20 15 10

02 1026 1332 1759 2500

03 1990 2340 2600 3100 3340 3600

N2 1305

N02 1900 2410 2440 3985

HN02 3970

N205 2050 3800

H202 2000 3800

HCHO 3600

HN03 1900 2100 3250 3700

N20 1680 2550 3340

H02 2450

N0 1217 2300

H20 1430 1980

CH4 800 1625

C02 900 1200 1475 1980

HCHO 3600

24

1 1 3 1.00

02 = 0 + 0 1759-2424

1 2 2 1.00

02 = 0 + 010 1332-1759

1 3 1 1.00

02 = 0 + 015 1026-1332

2 6 4 0.001

03 = 0 + 0210 3100-3340

2 7 3 1.00

03 = 010 + 0210 2600-3100

2 8 1 0.01

03 = 015 + 0210 1990-2370

2 9 2 0.05

03 = 0 + 0215 2340-2600

4 11 3 1.00

N02 + HV = 0 + N0 2440-3985

4 12 1 0.50

N02 + HV = 010 + N0 1900-2410

4 12 2 0.20

N02 + HV = 010 + N0 2410-2440

10 13 6 0.99

N20 + HV = 010 + N2 1680-3340

10 14 6 0.01

N20 + HV = N + N0 1680-2550

6 17 6 0.50

N205 + HV = 0 + N02 + N02

11 19 6 1.00

H02 + HV = 0 + OH

7 20 6 1.00

H202 + HV = OH + OH

15 21 2 1.00

C02 + HV = 0 + C0

15 22 1 1.00

C02 + HV = 010 + C0

14 23 6 0.33

CH4 + HV = H + CH3

14 24 6 0.67

CH4 + HV = H2 + CH2

8 25 6 1.00

HCHO + HV = H + CH0

16 26 6 1.00

HCHU + HV = H2 + C0

5 31 6 1.00

HN02 + HV = N0 + OH

9 32 6 1.00

HN03 + HV = N02 + OH 1900-3250

9 33 1 0.01

HN03 + HV = H + N03 11900-2100

.11700+21

02 OVER 75 KM.

.42300+15

02 70 KM.

.81900+15

02 65 KM.

.15000+16

02 60 KM.

.26200+16

02 55 KM.

.447300+16

02 50 KM.

.855000+16

02 45 KM.

.174000+17	02	40 KM.
.371000+17	02	35 KM.
.802000+17	02	30 KM.
.174600+18	02	25 KM.
.387400+18	02	20 KM.
.848700+18	02	15 KM.
.180000+19	02	10 KM.
.100000+14	03 OVER	75 KM.
1.000000+10	03	70 KM.
.19100+11	03	65 KM.
.31900+11	03	60 KM.
.70400+11	03	55 KM.
.800000+11	03	50 KM.
.250000+12	03	45 KM.
.700000+12	03	40 KM.
.151840+13	03	35 KM.
.352700+13	03	30 KM.
.500600+13	03	25 KM.
.399910+13	03	20 KM.
.224980+13	03	15 KM.
.100120+13	03	10 KM.
.43800+21	N2 OVER	75 KM.
.15800+16	N2	70 KM.
.30500+16	N2	65 KM.
.56000+16	N2	60 KM.
.97800+16	N2	55 KM.
.166700+17	N2	50 KM.
.319200+17	N2	45 KM.
.648800+17	N2	40 KM.
.137400+18	N2	35 KM.
.299000+18	N2	30 KM.
.650700+18	N2	25 KM.
.144400+19	N2	20 KM.
.316300+19	N2	15 KM.
.671300+19	N2	10 KM.
.0	N02 OVER	75 KM.
.10000+06	N02	70 KM.
.60000+06	N02	65 KM.
.20500+07	N02	60 KM.
.11000+08	N02	55 KM.
.200000+06	N02	50 KM.
.400000+08	N02	45 KM.
.400000+09	N02	40 KM.
.169710+10	N02	35 KM.
.253100+10	N02	30 KM.
.261050+10	N02	25 KM.
.184100+10	N02	20 KM.
.164560+10	N02	15 KM.
.172280+10	N02	10 KM.
.0	HN02 OVER	75 KM.
.10000E-02	HN02	70 KM.
.13000E-01	HN02	65 KM.
.31000E-01	HN02	60 KM.
.50000E-01	HN02	55 KM.
.566140+06	HN02	50 KM.
.300960+07	HN02	45 KM.



.111160+08	HN02	40 KM.
.162140+08	HN02	35 KM.
.137620+08	HN02	30 KM.
.103470+08	HN02	25 KM.
.994620+07	HN02	20 KM.
.140690+08	HN02	15 KM.
.164820+08	HN02	10 KM.
.0	N205 OVER	75 KM.
.18598-01	N205	70 KM.
.90000-01	N205	65 KM.
.17685+03	N205	60 KM.
.10000+04	N205	55 KM.
.907050+01	N205	50 KM.
.592310+04	N205	45 KM.
.175550+07	N205	40 KM.
.482650+08	N205	35 KM.
.228780+09	N205	30 KM.
.429510+09	N205	25 KM.
.325840+09	N205	20 KM.
.265800+09	N205	15 KM.
.268930+09	N205	10 KM.
.0	H202 OVER	75 KM.
.20000+05	H202	70 KM.
.60000+05	H202	65 KM.
.90000+05	H202	60 KM.
.20000+06	H202	55 KM.
.601700+07	H202	50 KM.
.112840+08	H202	45 KM.
.179810+08	H202	40 KM.
.241310+08	H202	35 KM.
.417810+08	H202	30 KM.
.421880+08	H202	25 KM.
.328470+08	H202	20 KM.
.297320+08	H202	15 KM.
.361450+08	H202	10 KM.
.0	HCHO OVER	75 KM.
.10000+06	HCHO	70 KM.
.40000+06	HCHO	65 KM.
.20000+05	HCHO	60 KM.
1.30000+05	HCHO	55 KM.
7.00000+06	HCHO	50 KM.
1.20000+07	HCHO	45 KM.
2.05000+07	HCHO	40 KM.
1.90000+07	HCHO	35 KM.
1.20000+07	HCHO	30 KM.
9.00000+06	HCHO	25 KM.
2.90000+07	HCHO	20 KM.
5.30000+07	HCHO	15 KM.
7.70000+07	HCHO	10 KM.
.0	HN03 OVER	75 KM.
1.00000+03	HN03	70 KM.
6.00000+03	HN03	65 KM.
1.50000+04	HN03	60 KM.
1.00000+05	HN03	55 KM.
.700000+05	HN03	50 KM.
.204670+07	HN03	45 KM.



.550000+08	HN03	40 KM.
.150000+09	HN03	35 KM.
.880450+09	HN03	30 KM.
.466300+10	HN03	25 KM.
.999410+10	HN03	20 KM.
.710190+10	HN03	15 KM.
.118550+10	HN03	10 KM.
0.0	N20 OVER	75 KM.
1.000000+04	N20	70 KM.
7.000000+04	N20	65 KM.
3.200000+05	N20	60 KM.
4.000000+06	N20	55 KM.
.100000+04	N20	50 KM.
.300000+06	N20	45 KM.
.130000+09	N20	40 KM.
.478090+10	N20	35 KM.
.407080+11	N20	30 KM.
.202340+12	N20	25 KM.
.598730+12	N20	20 KM.
.124980+13	N20	15 KM.
.239980+13	N20	10 KM.
.0	H02 OVER	75 KM.
.180000+05	H02	70 KM.
.380000+05	H02	65 KM.
.530000+06	H02	60 KM.
.130000+07	H02	55 KM.
.116420+08	H02	50 KM.
.168000+08	H02	45 KM.
.252060+08	H02	40 KM.
.507040+08	H02	35 KM.
.896060+08	H02	30 KM.
.102280+09	H02	25 KM.
.727910+08	H02	20 KM.
.538650+08	H02	15 KM.
.486180+08	H02	10 KM.
.0	NO OVER	75 KM.
.250000+08	NO	70 KM.
.830000+08	NO	65 KM.
.270000+09	NO	60 KM.
.760000+09	NO	55 KM.
.845760+09	NO	50 KM.
.161370+10	NO	45 KM.
.256370+10	NO	40 KM.
.263490+10	NO	35 KM.
.229750+10	NO	30 KM.
.189270+10	NO	25 KM.
.179760+10	NO	20 KM.
.266550+10	NO	15 KM.
.438570+10	NO	10 KM.
.0	H20 OVER	75 KM.
.50887+10	H20	70 KM.
.10000+11	H20	65 KM.
.16531+11	H20	60 KM.
.40000+11	H20	55 KM.
.116630+12	H20	50 KM.
.194340+12	H20	45 KM.

.343950+12	H20	40 KM.
.676180+12	H20	35 KM.
.144950+13	H20	30 KM.
.307780+13	H20	25 KM.
.731920+13	H20	20 KM.
.202050+14	H20	15 KM.
.103000+15	H20	10 KM.
.0	CH4 OVER	75 KM.
.15000+09	CH4	70 KM.
.40009+09	CH4	65 KM.
.09429+10	CH4	60 KM.
.23002+10	CH4	55 KM.
.596450+10	CH4	50 KM.
.168180+11	CH4	45 KM.
.467340+11	CH4	40 KM.
.129700+12	CH4	35 KM.
.324050+12	CH4	30 KM.
.809400+12	CH4	25 KM.
.189870+13	CH4	20 KM.
.480030+13	CH4	15 KM.
.103920+14	CH4	10 KM.
.0	C02 OVER	75 KM.
.52100+12	C02	70 KM.
.10000+13	C02	65 KM.
.20000+13	C02	60 KM.
.37009+13	C02	55 KM.
.725870+13	C02	50 KM.
.139010+14	C02	45 KM.
.283020+14	C02	40 KM.
.597930+14	C02	35 KM.
.130000+15	C02	30 KM.
.283000+15	C02	25 KM.
.629000+15	C02	20 KM.
.138000+16	C02	15 KM.
.292000+16	C02	10 KM.
.0	HCHO OVER	75 KM.
.10000+06	HCHO	70 KM.
.40000+06	HCHO	65 KM.
.20000+05	HCHO	60 KM.
1.30000+05	HCHO	55 KM.
7.00000+06	HCHO	50 KM.
1.20000+07	HCHO	45 KM.
2.05000+07	HCHO	40 KM.
1.90000+07	HCHO	35 KM.
1.20000+07	HCHO	30 KM.
9.00000+06	HCHO	25 KM.
2.90000+07	HCHO	20 KM.
5.30000+07	HCHO	15 KM.
7.70000+07	HCHO	10 KM.
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1 0 1.00 1.00 1.00 1.00 1.00 1.00		

## 7. SAMPLE OF OUTPUT

Shown here is a sample printer output listing generated with the input data listed in Section 6.

LATITUDE			LONGITUDE		
DEG	MIN	SEC	DEG	MIN	SEC
65	0	0	106	0	0

LATITUDE = 1.13447 RADIANS  
 LONGITUDE = 1.85005 RADIANS

MONTH	DATE	TIME	INC
9	28	12.00	0

COSINE = .37693  
 SECANT = 2.65305  
 THETA = 1.18432 RADIANS OR 67.86164 DEGREES

SNL		
DEFN	=	T
PCH	=	F
ITAPE	=	T
IPHI	=	F
JAYS	=	T
DATA	=	F
SSUMIT	=	F
NFIL	=	+5000

SEND

THE NUMBER OF PHOTODISSOCIATION REACTIONS CONSIDERED IS 25



65 NORTH LATITUDE - SEPTEMBER 28 - 12 NOON

INTERVAL NCYCLE NPOS1 NPOS2 ISKIP

976 3975 30 950 0 0

NSPEC NTHETA NTOP NLAYER NWAVE LAYER(CM)

16 1 70 KM. 14 100 .500+06

CHEMICAL SYMBOLS

O2 O3 N2 NO2 HNO2 N2O5 H2O2 HCHO HNO3 N2O HO2  
NO H2O CH4 CO2 HCHO

ISKIP = 0 IS THE NUMBER OF LAYERS FOR WHICH RATES WILL NOT BE COMPUTED

NSPEC = 4 IS THE NUMBER OF ATTENUATING SPECIES ABOVE MODEL

COLUMN DENSITIES ABOVE 70 KM.

.117000+21	O2 OVER	70
.100000+14	O3 OVER	70
.438000+21	N2 OVER	70
.000000	NO2 OVER	70

NUMBER DENSITIES SPECIE ALTITUDE

.423000+15	O2	70 KM.
.819000+15	O2	65 KM.
.150000+16	O2	60 KM.
.262000+16	O2	55 KM.
.398000+16	O2	50 KM.
.838000+16	O2	45 KM.
.180000+17	O2	40 KM.
.377000+17	O2	35 KM.
.836000+17	O2	30 KM.
.177000+18	O2	25 KM.
.380000+18	O2	20 KM.
.810000+18	O2	15 KM.
.178000+19	O2	10 KM.

.100000+11	O3	70 KM.
.191000+11	O3	65 KM.
.319000+11	O3	60 KM.
.704000+11	O3	55 KM.
.221740+11	O3	50 KM.
.100170+12	O3	45 KM.
.475800+12	O3	40 KM.
.118340+13	O3	35 KM.
.213690+13	O3	30 KM.
.382660+13	O3	25 KM.
.526950+13	O3	20 KM.
.399940+13	O3	15 KM.

.212950+13	03	10 KM.
.158000+16	N2	70 KM.
.305000+16	N2	65 KM.
.560000+16	N2	60 KM.
.978000+16	N2	55 KM.
.142000+17	N2	50 KM.
.312000+17	N2	45 KM.
.672000+17	N2	40 KM.
.141000+18	N2	35 KM.
.312000+18	N2	30 KM.
.661000+18	N2	25 KM.
.142000+19	N2	20 KM.
.302000+19	N2	15 KM.
.664000+19	N2	10 KM.
.100000+06	N02	70 KM.
.600000+06	N02	65 KM.
.205000+07	N02	60 KM.
.110000+08	N02	55 KM.
.130920+08	N02	50 KM.
.722310+08	N02	45 KM.
.388110+09	N02	40 KM.
.114690+10	N02	35 KM.
.256170+10	N02	30 KM.
.363700+10	N02	25 KM.
.350680+10	N02	20 KM.
.155680+10	N02	15 KM.
.203900+10	N02	10 KM.
.100000-02	HN02	70 KM.
.130000-01	HN02	65 KM.
.310000-01	HN02	60 KM.
.500000-01	HN02	55 KM.
.438840+06	HN02	50 KM.
.185250+07	HN02	45 KM.
.531230+07	HN02	40 KM.
.127130+08	HN02	35 KM.
.689250+07	HN02	30 KM.
.407420+07	HN02	25 KM.
.308240+07	HN02	20 KM.
.180320+07	HN02	15 KM.
.176700+07	HN02	10 KM.
.185980-01	N205	70 KM.
.400000-01	N205	65 KM.
.176850+03	N205	60 KM.
.100000+04	N205	55 KM.
.114380+02	N205	50 KM.
.180820+04	N205	45 KM.
.263270+06	N205	40 KM.
.516550+07	N205	35 KM.
.849140+08	N205	30 KM.

.387780+09	N205	25 KM.
.569940+09	N205	20 KM.
.344980+09	N205	15 KM.
.595550+09	N205	10 KM.

.200000+05	H202	70 KM.
.600000+05	H202	65 KM.
.900000+05	H202	60 KM.
.200000+06	H202	55 KM.
.183080+08	H202	50 KM.
.629110+08	H202	45 KM.
.128910+09	H202	40 KM.
.357970+09	H202	35 KM.
.136850+09	H202	30 KM.
.474320+08	H202	25 KM.
.223400+08	H202	20 KM.
.168130+08	H202	15 KM.
.952830+07	H202	10 KM.

.100000+06	HCHO	70 KM.
.400000+06	HCHO	65 KM.
.620000+06	HCHO	60 KM.
.130000+06	HCHO	55 KM.
.994740+06	HCHO	50 KM.
.389200+07	HCHO	45 KM.
.100990+08	HCHO	40 KM.
.145000+08	HCHO	35 KM.
.135840+08	HCHO	30 KM.
.116880+08	HCHO	25 KM.
.100540+08	HCHO	20 KM.
.118130+08	HCHO	15 KM.
.141180+08	HCHO	10 KM.

.100000+04	HN03	70 KM.
.600000+04	HN03	65 KM.
.150000+05	HN03	60 KM.
.100000+06	HN03	55 KM.
.988650+06	HN03	50 KM.
.276050+07	HN03	45 KM.
.338950+08	HN03	40 KM.
.316850+09	HN03	35 KM.
.264360+10	HN03	30 KM.
.600150+10	HN03	25 KM.
.130100+11	HN03	20 KM.
.139930+11	HN03	15 KM.
.302020+10-	HN03	10 KM.

.100000+05	N20	70 KM.
.700000+05	N20	65 KM.
.320000+06	N20	60 KM.
.400000+07	N20	55 KM.
.447640+05	N20	50 KM.
.333020+06	N20	45 KM.

.129980+09	N20	40 KM.
.478100+10	N20	35 KM.
.407080+11	N20	30 KM.
.202340+12	N20	25 KM.
.598730+12	N20	20 KM.
.124980+13	N20	15 KM.
.239980+13	N20	10 KM.

.180000+05	H02	70 KM.
.380000+05	H02	65 KM.
.530000+06	H02	60 KM.
.130000+07	H02	55 KM.
.208300+08	H02	50 KM.
.381010+08	H02	45 KM.
.676660+08	H02	40 KM.
.112910+09	H02	35 KM.
.141820+09	H02	30 KM.
.104200+09	H02	25 KM.
.759600+08	H02	20 KM.
.572130+08	H02	15 KM.
.375550+08	H02	10 KM.

.250000+08	NO	70 KM.
.830000+08	NO	65 KM.
.270000+09	NO	60 KM.
.760000+09	NO	55 KM.
.145610+10	NO	50 KM.
.166860+10	NO	45 KM.
.189690+10	NO	40 KM.
.326200+10	NO	35 KM.
.320000+10	NO	30 KM.
.282990+10	NO	25 KM.
.205720+10	NO	20 KM.
.109270+10	NO	15 KM.
.194880+10	NO	10 KM.

.508870+10	H20	70 KM.
.100000+11	H20	65 KM.
.165310+11	H20	60 KM.
.400000+11	H20	55 KM.
.762420+11	H20	50 KM.
.221080+12	H20	45 KM.
.413120+12	H20	40 KM.
.576170+12	H20	35 KM.
.124020+13	H20	30 KM.
.288010+13	H20	25 KM.
.705010+13	H20	20 KM.
.147000+14	H20	15 KM.
.255000+14	H20	10 KM.

.150000+09	CH4	70 KM.
.400090+09	CH4	65 KM.
.942900+09	CH4	60 KM.



.230020+10	CH4	55 KM.
.474770+10	CH4	50 KM.
.124870+11	CH4	45 KM.
.349820+11	CH4	40 KM.
.100000+12	CH4	35 KM.
.279000+12	CH4	30 KM.
.750000+12	CH4	25 KM.
.150000+13	CH4	20 KM.
.348000+13	CH4	15 KM.
.750000+13	CH4	10 KM.

.521000+12	CO2	70 KM.
.100000+13	CO2	65 KM.
.200000+13	CO2	60 KM.
.370090+13	CO2	55 KM.
.597010+13	CO2	50 KM.
.126000+14	CO2	45 KM.
.270010+14	CO2	40 KM.
.565000+14	CO2	35 KM.
.125000+15	CO2	30 KM.
.266000+15	CO2	25 KM.
.569000+15	CO2	20 KM.
.121000+16	CO2	15 KM.
.267000+16	CO2	10 KM.

.100000+06	HCHO	70 KM.
.400000+06	HCHO	65 KM.
.620000+06	HCHO	60 KM.
.130000+06	HCHO	55 KM.
.994760+06	HCHO	50 KM.
.389200+07	HCHO	45 KM.
.103990+08	HCHO	40 KM.
.145000+08	HCHO	35 KM.
.135840+08	HCHO	30 KM.
.116880+08	HCHO	25 KM.
.100540+08	HCHO	20 KM.
.118130+08	HCHO	15 KM.
.141180+08	HCHO	10 KM.

SPECIE	PHI I	PHI
02	.100+01	.100+01
03	.100+01	.100+01
N2	.100+01	.100+01
N02	.100+01	.100+01
HN02	.100+01	.100+01
N205	.100+01	.100+01
H202	.100+01	.100+01
HCHO	.100+01	.100+01
HN03	.100+01	.100+01
N20	.100+01	.100+01
H02	.100+01	.100+01

NO	.100+01	.100+01
H2O	.100+01	.100+01
CH4	.100+01	.100+01
CO2	.100+01	.100+01
HCHO	.100+01	.100+01

MODEL LAYERS CENTERED AT FOLLOWING ALTITUDES

70	65	60	55	50	45	40	35	30	25	20	15	10
----	----	----	----	----	----	----	----	----	----	----	----	----

JJ = 1 DZ = .133+07

MODEL LAYER = 2	ALTITUDE = 70 KM.	DX = .1327+07
MODEL LAYER = 3	ALTITUDE = 65 KM.	DX = .1327+07
MODEL LAYER = 4	ALTITUDE = 60 KM.	DX = .1327+07
MODEL LAYER = 5	ALTITUDE = 55 KM.	DX = .1327+07
MODEL LAYER = 6	ALTITUDE = 50 KM.	DX = .1327+07
MODEL LAYER = 7	ALTITUDE = 45 KM.	DX = .1327+07
MODEL LAYER = 8	ALTITUDE = 40 KM.	DX = .1327+07
MODEL LAYER = 9	ALTITUDE = 35 KM.	DX = .1327+07
MODEL LAYER = 10	ALTITUDE = 30 KM.	DX = .1327+07
MODEL LAYER = 11	ALTITUDE = 25 KM.	DX = .1327+07
MODEL LAYER = 12	ALTITUDE = 20 KM.	DX = .1327+07
MODEL LAYER = 13	ALTITUDE = 15 KM.	DX = .1327+07
MODEL LAYER = 14	ALTITUDE = 10 KM.	DX = .1327+07

SPECIE	EQN.	RATE	EFF.	CHEMICAL REACTION
1	1	3	1.000	02 = 0 + 0 1759-2424
1	2	2	1.000	02 = 0 + 010 1332-1759
1	3	1	1.000	02 = 0 + 015 1026-1332
2	6	4	0.001	03 = 0 + 0210 3100-3340
2	7	3	1.000	03 = 010 + 0210 2600-3100
2	8	1	.010	03 = 015 + 0210 1990-2370
2	9	2	.050	03 = 0 + 0215 2340-2600
4	11	3	1.000	N02 + HV = 0 + N0 2440-3985
4	12	1	.500	N02 + HV = 010 + N0 1900-2410
4	12	2	.200	N02 + HV = 010 + N0 2410-2440
10	13	6	.990	N20 + HV = 010 + N2 1680-3340
10	14	6	.010	N20 + HV = N + N0 1680-2550
6	17	6	.500	N205 + HV = 0 + N02 + N02
11	19	6	1.000	H02 + HV = 0 + OH.
7	20	6	1.000	H202 + HV = OH + OH
15	21	2	1.000	C02 + HV = 0 + C0
15	22	1	1.000	C02 + HV = 010 + C0
14	23	6	.330	CH4 + HV = H + CH3
14	24	6	.670	CH4 + HV = H2 + CH2
8	25	6	1.000	HCHO + HV = H + CHO
16	26	6	1.000	HCHO + HV = H2 + C0
5	31	6	1.000	HN02 + HV = N0 + OH
9	32	6	1.000	HN03 + HV = N02 + OH 1900-3250
9	33	1	.010	HN03 + HV = H + N03 11900-2100

THE FOLLOWING ARE THE WAVELENGTH INTERVALS  
OVER WHICH THE PER ANGSTROM CONTRIBUTIONS  
ARE SUMMED FOR DIFFERENT PHOTO-DISSOCIATION  
PROCESSES:

02	976	1332	1759	2500	0	0
03	976	2340	2600	3100	3340	3600
N2	976	977	0	0	0	0
N02	976	2410	2440	3975	0	0
HN02	976	977	0	0	0	0
N205	976	3800	0	0	0	0
H202	976	3800	0	0	0	0
HCHO	976	977	0	0	0	0
HN03	976	2100	3250	3700	0	0
N20	976	2550	3340	0	0	0
H02	976	977	0	0	0	0
N0	976	2300	0	0	0	0
H20	976	1980	0	0	0	0
CH4	976	1625	0	0	0	0
C02	976	1200	1475	1980	0	0
HCHO	976	977	0	0	0	0



SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.3411-10	.0000	.7324-09	.0000	.7665-09
O3	.1752-05	.1883-03	.8363-03	.1908-02	.2198-05	.2936-02
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.3142-05	.2920-04	.2924-02	.0000	.0000	.2956-02
HN02	.1980-03	.0000	.0000	.0000	.0000	.1980-03
N205	.1896-06	.1814-03	.0000	.0000	.0000	.1815-03
H202	.2543-05	.4881-04	.0000	.0000	.0000	.5135-04
HCHO	.8960-04	.0000	.0000	.0000	.0000	.8960-04
HN03	.4025-04	.1426-04	.1958-05	.0000	.0000	.5647-04
N20	.8719-08	.5400-06	.0000	.0000	.0000	.5487-06
H02	.2164-04	.0000	.0000	.0000	.0000	.2164-04
N0	.6231-08	.1360-05	.0000	.0000	.0000	.1367-05
H20	.1452-06	.0000	.0000	.0000	.0000	.1452-06
CH4	.0000	.1409-07	.4228-07	.0000	.0000	.5638-07
CO2	.0000	.1237-08	.0000	.0000	.0000	.1237-08
HCHO	.5981-04	.0000	.0000	.0000	.0000	.5981-04

ALTITUDE = 70 KM.

1	.73-09	70 KM.
2	.10-22	70 KM.
3	.34-10	70 KM.
6	.22-08	70 KM.
7	.19-02	70 KM.
8	.19-05	70 KM.
9	.42-04	70 KM.
11	.29-02	70 KM.
12	.15-04	70 KM.
13	.53-06	70 KM.
14	.54-08	70 KM.
15	.17-02	70 KM.
16	.27-02	70 KM.
17	.91-04	70 KM.
19	.22-04	70 KM.
20	.49-04	70 KM.
21	.12-08	70 KM.
22	.10-22	70 KM.
23	.14-07	70 KM.
24	.42-07	70 KM.
25	.90-04	70 KM.
26	.60-04	70 KM.
31	.20-03	70 KM.
32	.56-04	70 KM.
33	.56-06	70 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
02	.0000	.9150-13	.0000	.5085-09	.0000	.5086-09
03	.1272-05	.1611-03	.6811-03	.1624-02	.1966-05	.2469-02
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.1601-05	.2522-04	.2707-02	.0000	.0000	.2734-02
HN02	.1842-03	.0000	.0000	.0000	.0000	.1842-03
N205	.1875-06	.1581-03	.0000	.0000	.0000	.1583-03
H202	.2171-05	.4278-04	.0000	.0000	.0000	.4495-04
HCHO	.8304-04	.0000	.0000	.0000	.0000	.8304-04
HN03	.3455-04	.1219-04	.1776-05	.0000	.0000	.4852-04
N20	.2436-10	.4193-06	.0000	.0000	.0000	.4193-06
H02	.1878-04	.0000	.0000	.0000	.0000	.1878-04
N0	.1753-10	.1191-05	.0000	.0000	.0000	.1191-05
H20	.4367-07	.0000	.0000	.0000	.0000	.4367-07
CH4	.0000	.3955-10	.1186-09	.0000	.0000	.1582-09
C02	.0000	.4949-09	.0000	.0000	.0000	.4949-09
HCHO	.5504-04	.0000	.0000	.0000	.0000	.5504-04

AltITUDE = 65 KM.

1	.51-09	65 KM.
2	.10-22	65 KM.
3	.91-13	65 KM.
6	.20-08	65 KM.
7	.16-02	65 KM.
8	.16-05	65 KM.
9	.34-04	65 KM.
11	.27-02	65 KM.
12	.13-04	65 KM.
13	.42-06	65 KM.
14	.42-08	65 KM.
15	.17-02	65 KM.
16	.27-02	65 KM.
17	.79-04	65 KM.
19	.19-04	65 KM.
20	.43-04	65 KM.
21	.49-09	65 KM.
22	.10-22	65 KM.
23	.40-10	65 KM.
24	.12-09	65 KM.
25	.83-04	65 KM.
26	.55-04	65 KM.
31	.18-03	65 KM.
32	.49-04	65 KM.
33	.49-06	65 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.6797-17	.0000	.4143-09	.0000	.4143-09
O3	.1154-05	.1421-03	.5213-03	.1397-02	.1949-05	.2064-02
N2	.0000	.0000	.0000	.0000	.0000	.0000
NO2	.1182-05	.2302-04	.2693-02	.0000	.0000	.2717-02
HN02	.1836-03	.0000	.0000	.0000	.0000	.1836-03
N2O5	.1837-06	.1431-03	.0000	.0000	.0000	.1433-03
H2O2	.2043-05	.3906-04	.0000	.0000	.0000	.4110-04
HCHO	.8249-04	.0000	.0000	.0000	.0000	.8249-04
HN03	.3216-04	.1091-04	.1738-05	.0000	.0000	.4481-04
N2O	.8581-14	.3802-06	.0000	.0000	.0000	.3802-06
H02	.1701-04	.0000	.0000	.0000	.0000	.1701-04
NO	.2612-14	.1111-05	.0000	.0000	.0000	.1111-05
H2O	.2911-07	.0000	.0000	.0000	.0000	.2911-07
CH4	.0000	.4906-14	.1472-13	.0000	.0000	.1962-13
CO2	.0000	.3936-09	.0000	.0000	.0000	.3936-09
HCHO	.5437-04	.0000	.0000	.0000	.0000	.5437-04

ALTITUDE = 60 KM.

1	.41-09	60 KM.
2	.10-22	60 KM.
3	.68-17	60 KM.
6	.19-08	60 KM.
7	.14-02	60 KM.
8	.14-05	60 KM.
9	.26-04	60 KM.
11	.27-02	60 KM.
12	.12-04	60 KM.
13	.38-06	60 KM.
14	.38-08	60 KM.
15	.17-02	60 KM.
16	.27-02	60 KM.
17	.72-04	60 KM.
19	.17-04	60 KM.
20	.39-04	60 KM.
21	.39-09	60 KM.
22	.10-22	60 KM.
23	.49-14	60 KM.
24	.15-13	60 KM.
25	.82-04	60 KM.
26	.54-04	60 KM.
31	.18-03	60 KM.
32	.45-04	60 KM.
33	.45-06	60 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
02	.0000	.1657-21	.0000	.3138-09	.0000	.3138-09
03	.1023-05	.1174-03	.3365-03	.1111-02	.1931-05	.1568-02
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.8083-06	.2021-04	.2677-02	.0000	.0000	.2698-02
HN02	.1829-03	.0000	.0000	.0000	.0000	.1829-03
N205	.1771-06	.1245-03	.0000	.0000	.0000	.1246-03
H202	.1881-05	.3444-04	.0000	.0000	.0000	.3632-04
HCHO	.8187-04	.0000	.0000	.0000	.0000	.8187-04
HN03	.2928-04	.9307-05	.1685-05	.0000	.0000	.4027-04
N20	.2403-18	.3352-06	.0000	.0000	.0000	.3352-06
H02	.1477-04	.0000	.0000	.0000	.0000	.1477-04
N0	.6974-19	.1005-05	.0000	.0000	.0000	.1005-05
H20	.1757-07	.0000	.0000	.0000	.0000	.1757-07
CH4	.0000	.1287-18	.3861-18	.0000	.0000	.5148-18
C02	.0000	.2949-09	.0000	.0000	.0000	.2949-09
HCHO	.5351-04	.0000	.0000	.0000	.0000	.5351-04

ALTITUDE = 55 KM.

1	.31-09	55 KM.
2	.10-22	55 KM.
3	.17-21	55 KM.
6	.19-08	55 KM.
7	.11-02	55 KM.
8	.12-05	55 KM.
9	.17-04	55 KM.
11	.27-02	55 KM.
12	.10-04	55 KM.
13	.33-06	55 KM.
14	.34-08	55 KM.
15	.17-02	55 KM.
16	.27-02	55 KM.
17	.62-04	55 KM.
19	.15-04	55 KM.
20	.34-04	55 KM.
21	.29-09	55 KM.
22	.10-22	55 KM.
23	.13-18	55 KM.
24	.39-18	55 KM.
25	.82-04	55 KM.
26	.54-04	55 KM.
31	.18-03	55 KM.
32	.40-04	55 KM.
33	.40-06	55 KM.



SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.1630-29	.0000	.2168-09	.0000	.2168-09
O3	.8752-06	.8130-04	.1314-03	.7266-03	.1915-05	.9421-03
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.5040-06	.1611-04	.2663-02	.0000	.0000	.2680-02
HN02	.1827-03	.0000	.0000	.0000	.0000	.1827-03
N205	.1652-06	.9914-04	.0000	.0000	.0000	.9930-04
H202	.1671-05	.2829-04	.0000	.0000	.0000	.2996-04
HCH0	.8124-04	.0000	.0000	.0000	.0000	.8124-04
HN03	.2591-04	.7122-05	.1598-05	.0000	.0000	.3463-04
N20	.2364-26	.2841-06	.0000	.0000	.0000	.2841-06
H02	.1165-04	.0000	.0000	.0000	.0000	.1165-04
N0	.6863-27	.8522-06	.0000	.0000	.0000	.8522-06
H20	.9809-08	.0000	.0000	.0000	.0000	.9809-08
CH4	.0000	.1267-26	.3800-26	.0000	.0000	.5066-26
C02	.0000	.2032-09	.0000	.0000	.0000	.2032-09
HCH0	.5225-04	.0000	.0000	.0000	.0000	.5225-04

ALTITUDE = 50 KM.

1	.22-09	50 KM.
2	.10-22	50 KM.
3	.16-29	50 KM.
6	.19-08	50 KM.
7	.73-03	50 KM.
8	.81-06	50 KM.
9	.66-05	50 KM.
11	.27-02	50 KM.
12	.81-05	50 KM.
13	.28-06	50 KM.
14	.28-08	50 KM.
15	.17-02	50 KM.
16	.27-02	50 KM.
17	.50-04	50 KM.
19	.12-04	50 KM.
20	.28-04	50 KM.
21	.20-09	50 KM.
22	.10-22	50 KM.
23	.13-26	50 KM.
24	.38-26	50 KM.
25	.81-04	50 KM.
26	.52-04	50 KM.
31	.18-03	50 KM.
32	.35-04	50 KM.
33	.35-06	50 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.1664-09	.0000	.1664-09
O3	.7495-06	.7181-04	.9775-04	.6462-03	.1907-05	.8184-03
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.3110-06	.1473-04	.2658-02	.0000	.0000	.2673-02
HN02	.1826-03	.0000	.0000	.0000	.0000	.1826-03
N205	.1542-06	.9224-04	.0000	.0000	.0000	.9240-04
H202	.1473-05	.2674-04	.0000	.0000	.0000	.2821-04
HCH0	.8099-04	.0000	.0000	.0000	.0000	.8099-04
HN03	.2305-04	.6542-05	.1570-05	.0000	.0000	.3116-04
N20	.0000	.2435-06	.0000	.0000	.0000	.2435-06
H02	.1059-04	.0000	.0000	.0000	.0000	.1059-04
N0	.0000	.7787-06	.0000	.0000	.0000	.7787-06
H20	.5725-08	.0000	.0000	.0000	.0000	.5725-08
CH4	.0000	.0000	.0000	.0000	.0000	.0000
CO2	.0000	.1383-09	.0000	.0000	.0000	.1383-09
HCH0	.5182-04	.0000	.0000	.0000	.0000	.5182-04

ALTITUDE = 45 KM.

1	.17-09	45 KM.
2	.10-22	45 KM.
3	.10-22	45 KM.
6	.19-08	45 KM.
7	.65-03	45 KM.
8	.72-06	45 KM.
9	.49-05	45 KM.
11	.27-02	45 KM.
12	.74-05	45 KM.
13	.24-06	45 KM.
14	.24-08	45 KM.
15	.17-02	45 KM.
16	.27-02	45 KM.
17	.46-04	45 KM.
19	.11-04	45 KM.
20	.27-04	45 KM.
21	.14-09	45 KM.
22	.10-22	45 KM.
23	.10-22	45 KM.
24	.10-22	45 KM.
25	.81-04	45 KM.
26	.52-04	45 KM.
31	.18-03	45 KM.
32	.31-04	45 KM.
33	.31-06	45 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.1103-09	.0000	.1103-09
O3	.5635-06	.4440-04	.2643-04	.4199-03	.1887-05	.4932-03
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.1445-06	.1096-04	.2645-02	.0000	.0000	.2657-02
HN02	.1823-03	.0000	.0000	.0000	.0000	.1823-03
N205	.1303-06	.7297-04	.0000	.0000	.0000	.7310-04
H202	.1134-05	.2253-04	.0000	.0000	.0000	.2366-04
HCHO	.8019-04	.0000	.0000	.0000	.0000	.8019-04
HN03	.1836-04	.4884-05	.1461-05	.0000	.0000	.2470-04
N20	.0000	.1844-06	.0000	.0000	.0000	.1844-06
H02	.7886-05	.0000	.0000	.0000	.0000	.7886-05
N0	.0000	.5989-06	.0000	.0000	.0000	.5989-06
H20	.2750-08	.0000	.0000	.0000	.0000	.2750-08
CH4	.0000	.0000	.0000	.0000	.0000	.0000
CO2	.0000	.7511-10	.0000	.0000	.0000	.7511-10
HCHO	.5022-04	.0000	.0000	.0000	.0000	.5022-04

ALTITUDE = 40 KM.

1	.11-09	40 KM.
2	.10-22	40 KM.
3	.10-22	40 KM.
6	.19-08	40 KM.
7	.42-03	40 KM.
8	.44-06	40 KM.
9	.13-05	40 KM.
11	.26-02	40 KM.
12	.55-05	40 KM.
13	.18-06	40 KM.
14	.18-08	40 KM.
15	.17-02	40 KM.
16	.27-02	40 KM.
17	.36-04	40 KM.
19	.79-05	40 KM.
20	.23-04	40 KM.
21	.75-10	40 KM.
22	.10-22	40 KM.
23	.10-22	40 KM.
24	.10-22	40 KM.
25	.80-04	40 KM.
26	.50-04	40 KM.
31	.18-03	40 KM.
32	.25-04	40 KM.
33	.25-06	40 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
02	.0000	.0000	.0000	.4605-10	.0000	.4605-10
03	.3014-06	.9083-05	.8908-07	.1481-03	.1809-05	.1594-03
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.3803-07	.4244-05	.2614-02	.0000	.0000	.2618-02
HN02	.1817-03	.0000	.0000	.0000	.0000	.1817-03
N205	.8090-07	.3975-04	.0000	.0000	.0000	.3983-04
H202	.6160-06	.1593-04	.0000	.0000	.0000	.1655-04
HCH0	.7729-04	.0000	.0000	.0000	.0000	.7729-04
HN03	.1045-04	.2034-05	.1082-05	.0000	.0000	.1357-04
N20	.0000	.9817-07	.0000	.0000	.0000	.9817-07
H02	.3342-05	.0000	.0000	.0000	.0000	.3342-05
N0	.0000	.2644-06	.0000	.0000	.0000	.2644-06
H20	.9305-09	.0000	.0000	.0000	.0000	.9305-09
CH4	.0000	.0000	.0000	.0000	.0000	.0000
C02	.0000	.2623-10	.0000	.0000	.0000	.2623-10
HCH0	.4448-04	.0000	.0000	.0000	.0000	.4448-04

ALTITUDE = 35 KM.

1	.46-10	35 KM.
2	.10-22	35 KM.
3	.10-22	35 KM.
6	.18-08	35 KM.
7	.15-03	35 KM.
8	.91-07	35 KM.
9	.45-08	35 KM.
11	.26-02	35 KM.
12	.21-05	35 KM.
13	.97-07	35 KM.
14	.98-09	35 KM.
15	.17-02	35 KM.
16	.27-02	35 KM.
17	.20-04	35 KM.
19	.33-05	35 KM.
20	.16-04	35 KM.
21	.26-10	35 KM.
22	.10-22	35 KM.
23	.10-22	35 KM.
24	.10-22	35 KM.
25	.77-04	35 KM.
26	.44-04	35 KM.
31	.18-03	35 KM.
32	.14-04	35 KM.
33	.14-06	35 KM.



SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.1142-10	.0000	.1142-10
O3	.8604-07	.1070-05	.6027-12	.4403-04	.1636-05	.4682-04
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.3668-08	.8360-06	.2573-02	.0000	.0000	.2574-02
HN02	.1806-03	.0000	.0000	.0000	.0000	.1806-03
N205	.2747-07	.1894-04	.0000	.0000	.0000	.1897-04
H202	.1802-06	.1201-04	.0000	.0000	.0000	.1219-04
HCH0	.7247-04	.0000	.0000	.0000	.0000	.7247-04
HN03	.3119-05	.4276-06	.6221-06	.0000	.0000	.4169-05
N20	.0000	.2780-07	.0000	.0000	.0000	.2780-07
H02	.7795-06	.0000	.0000	.0000	.0000	.7795-06
N0	.0000	.5798-07	.0000	.0000	.0000	.5798-07
H20	.1588-09	.0000	.0000	.0000	.0000	.1588-09
CH4	.0000	.0000	.0000	.0000	.0000	.0000
CO2	.0000	.4213-11	.0000	.0000	.0000	.4213-11
HCH0	.3648-04	.0000	.0000	.0000	.0000	.3648-04

ALTITUDE = 30 KM.

1	.11-10	30 KM.
2	.10-22	30 KM.
3	.10-22	30 KM.
6	.16-08	30 KM.
7	.44-04	30 KM.
8	.11-07	30 KM.
9	.30-13	30 KM.
11	.26-02	30 KM.
12	.42-06	30 KM.
13	.28-07	30 KM.
14	.28-09	30 KM.
15	.17-02	30 KM.
16	.27-02	30 KM.
17	.95-05	30 KM.
19	.78-06	30 KM.
20	.12-04	30 KM.
21	.42-11	30 KM.
22	.10-22	30 KM.
23	.10-22	30 KM.
24	.10-22	30 KM.
25	.72-04	30 KM.
26	.36-04	30 KM.
31	.18-03	30 KM.
32	.42-05	30 KM.
33	.42-07	30 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
02	.0000	.0000	.0000	.1043-11	.0000	.1043-11
03	.8226-08	.6452-07	.9845-21	.1210-04	.1368-05	.1354-04
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.3853-10	.6484-07	.2530-02	.0000	.0000	.2530-02
HN02	.1789-03	.0000	.0000	.0000	.0000	.1789-03
N205	.3100-08	.1182-04	.0000	.0000	.0000	.1183-04
H202	.1821-07	.1019-04	.0000	.0000	.0000	.1021-04
HCH0	.6723-04	.0000	.0000	.0000	.0000	.6723-04
HN03	.3067-06	.3462-07	.3415-06	.0000	.0000	.6828-06
N20	.0000	.2972-08	.0000	.0000	.0000	.2972-08
H02	.6936-07	.0000	.0000	.0000	.0000	.6936-07
N0	.0000	.4084-08	.0000	.0000	.0000	.4084-08
H20	.7439-11	.0000	.0000	.0000	.0000	.7439-11
CH4	.0000	.0000	.0000	.0000	.0000	.0000
C02	.0000	.1554-12	.0000	.0000	.0000	.1554-12
HCH0	.2988-04	.0000	.0000	.0000	.0000	.2988-04

ALTITUDE = 25 KM.

1	.10-11	25 KM.
2	.10-22	25 KM.
3	.10-22	25 KM.
6	.14-08	25 KM.
7	.12-04	25 KM.
8	.65-09	25 KM.
9	.49-22	25 KM.
11	.25-02	25 KM.
12	.32-07	25 KM.
13	.29-08	25 KM.
14	.30-10	25 KM.
15	.17-02	25 KM.
16	.27-02	25 KM.
17	.59-05	25 KM.
19	.69-07	25 KM.
20	.10-04	25 KM.
21	.16-12	25 KM.
22	.10-22	25 KM.
23	.10-22	25 KM.
24	.10-22	25 KM.
25	.67-04	25 KM.
26	.30-04	25 KM.
31	.18-03	25 KM.
32	.68-06	25 KM.
33	.68-08	25 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.1283-13	.0000	.1283-13
O3	.1103-09	.6297-09	.0000	.2901-05	.1004-05	.3906-05
N2	.0000	.0000	.0000	.0000	.0000	.0000
NO2	.8713-14	.7299-09	.2481-02	.0000	.0000	.2481-02
HNO2	.1764-03	.0000	.0000	.0000	.0000	.1764-03
N2O5	.4161-10	.9368-05	.0000	.0000	.0000	.9368-05
H2O2	.2702-09	.9027-05	.0000	.0000	.0000	.9027-05
HCHO	.6154-04	.0000	.0000	.0000	.0000	.6154-04
HNO3	.4140-08	.4259-09	.1838-06	.0000	.0000	.1884-06
N2O	.0000	.2407-09	.0000	.0000	.0000	.2407-09
HO2	.8631-09	.0000	.0000	.0000	.0000	.8631-09
NO	.0000	.3702-10	.0000	.0000	.0000	.3702-10
H2O	.4989-13	.0000	.0000	.0000	.0000	.4989-13
CH4	.0000	.0000	.0000	.0000	.0000	.0000
CO2	.0000	.5987-15	.0000	.0000	.0000	.5987-15
HCHO	.2438-04	.0000	.0000	.0000	.0000	.2438-04

Altitude = 20 KM.

1	.13-13	20 KM.
2	.10-22	20 KM.
3	.10-22	20 KM.
6	.10-08	20 KM.
7	.29-05	20 KM.
8	.63-11	20 KM.
9	.10-22	20 KM.
11	.25-02	20 KM.
12	.36-09	20 KM.
13	.24-09	20 KM.
14	.24-11	20 KM.
15	.17-02	20 KM.
16	.27-02	20 KM.
17	.47-05	20 KM.
19	.86-09	20 KM.
20	.90-05	20 KM.
21	.60-15	20 KM.
22	.10-22	20 KM.
23	.10-22	20 KM.
24	.10-22	20 KM.
25	.62-04	20 KM.
26	.24-04	20 KM.
31	.18-03	20 KM.
32	.19-06	20 KM.
33	.19-08	20 KM.

SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.6338-17	.0000	.6338-17
O3	.5440-13	.3874-12	.0000	.7953-06	.6677-06	.1463-05
N2	.0000	.0000	.0000	.0000	.0000	.0000
NO2	.9714-21	.4089-12	.2435-02	.0000	.0000	.2435-02
HNO2	.1738-03	.0000	.0000	.0000	.0000	.1738-03
N2O5	.1455-13	.7974-05	.0000	.0000	.0000	.7974-05
H2O2	.1546-12	.8180-05	.0000	.0000	.0000	.8180-05
HCHO	.5651-04	.0000	.0000	.0000	.0000	.5651-04
HN03	.2072-11	.2974-12	.1042-06	.0000	.0000	.1042-06
N2O	.0000	.9571-10	.0000	.0000	.0000	.9571-10
HO2	.4675-12	.0000	.0000	.0000	.0000	.4675-12
NO	.0000	.1689-13	.0000	.0000	.0000	.1689-13
H2O	.1411-16	.0000	.0000	.0000	.0000	.1411-16
CH4	.0000	.0000	.0000	.0000	.0000	.0000
CO2	.0000	.1007-18	.0000	.0000	.0000	.1007-18
HCHO	.2038-04	.0000	.0000	.0000	.0000	.2038-04

ALTITUDE = 15 KM.

1	.63-17	15 KM.
2	.10-22	15 KM.
3	.10-22	15 KM.
6	.67-09	15 KM.
7	.80-06	15 KM.
8	.39-14	15 KM.
9	.10-22	15 KM.
11	.24-02	15 KM.
12	.20-12	15 KM.
13	.95-10	15 KM.
14	.96-12	15 KM.
15	.17-02	15 KM.
16	.27-02	15 KM.
17	.40-05	15 KM.
19	.47-12	15 KM.
20	.82-05	15 KM.
21	.10-18	15 KM.
22	.10-22	15 KM.
23	.10-22	15 KM.
24	.10-22	15 KM.
25	.57-04	15 KM.
26	.20-04	15 KM.
31	.17-03	15 KM.
32	.10-06	15 KM.
33	.10-08	15 KM.



SYMB	SUM1	SUM2	SUM3	SUM4	SUM5	TOTAL
O2	.0000	.0000	.0000	.4932-21	.0000	.4932-21
O3	.1311-18	.1124-15	.0000	.3622-06	.4971-06	.8593-06
N2	.0000	.0000	.0000	.0000	.0000	.0000
N02	.7653-34	.7568-16	.2408-02	.0000	.0000	.2408-02
HN02	.1722-03	.0000	.0000	.0000	.0000	.1722-03
N205	.1505-19	.7318-05	.0000	.0000	.0000	.7318-05
H202	.4626-18	.7750-05	.0000	.0000	.0000	.7750-05
HCH0	.5371-04	.0000	.0000	.0000	.0000	.5371-04
HN03	.5580-17	.7096-16	.7412-07	.0000	.0000	.7412-07
N20	.0000	.5708-10	.0000	.0000	.0000	.5708-10
H02	.5541-16	.0000	.0000	.0000	.0000	.5541-16
N0	.0000	.5266-17	.0000	.0000	.0000	.5266-17
H20	.1944-22	.0000	.0000	.0000	.0000	.1944-22
CH4	.0000	.0000	.0000	.0000	.0000	.0000
C02	.0000	.9539-25	.0000	.0000	.0000	.9539-25
HCH0	.1842-04	.0000	.0000	.0000	.0000	.1842-04

ALTITUDE = 10 KM.

1	.49-21	10 KM.
2	.10-22	10 KM.
3	.10-22	10 KM.
6	.50-09	10 KM.
7	.36-06	10 KM.
8	.11-17	10 KM.
9	.10-22	10 KM.
11	.24-02	10 KM.
12	.38-16	10 KM.
13	.57-10	10 KM.
14	.57-12	10 KM.
15	.17-02	10 KM.
16	.27-02	10 KM.
17	.37-05	10 KM.
19	.55-16	10 KM.
20	.77-05	10 KM.
21	.95-25	10 KM.
22	.10-22	10 KM.
23	.10-22	10 KM.
24	.10-22	10 KM.
25	.54-04	10 KM.
26	.18-04	10 KM.
31	.17-03	10 KM.
32	.74-07	10 KM.
33	.74-09	10 KM.



END OF COMPUTATION.

## REFERENCES

1. Collins, J. L., "A computer Model to Calculate Photodissociation Rates in the Upper Atmosphere", Interim Report IRI-74-UA-9, Electrical Engineering Department, The University of Texas at El Paso (1974).
2. Collins, J. L., "Calculated Photodissociation Coefficients and Solar Flux Intensities in the 10-70 Kilometer Interval," Special Report SP4-76-UA-26, Electrical Engineering Department, The University of Texas at El Paso (1976).
3. Brinkman, R. T., et. al., "A Digitalized Ultraviolet Spectrum", NASA Report No. 32-391 (1966).
4. Thakaevara, M. P., et. al., Applied Optics, 8, 6 (1969).
5. Ackerman, M., "Ultraviolet Solar Radiation Related to Mesospheric Processes," Aeronomica Acta, A, No. 77 (1970).
6. Broadfoot, A. L., Astrophysical Journal, 123 (1972).
7. Koller, Lewis R., Ultraviolet Radiation, John Wiley & Sons, Inc., New York, New York (1965).
8. Kerker, M., The Scattering of Light and Other Electromagnetic Radiation, Academic Press, New York, New York (1959).
9. Leighton, P. A., Photochemistry of Air Pollution, Academic Press, New York, New York (1961).
10. Leighton, P. A., and W. A. Perkins, "Solar Radiation, Absorption Rates, and Photochemical Primary Processes in Urban Air", Report 14 prepared for Air Pollution Foundation, Los Angeles, California (1956).
11. Smart, W. M., Text-Book on Spherical Astronomy, University Press, Cambridge, England (1959).

## APPENDIX A: AUXILIARY PROGRAMS AND FILES

Several auxiliary programs are required for data preparation and manipulation and for the plotting of input and output data. For the conveniences of the user, documentation and data set-up have been provided on comment cards at the beginning of each program's main routine.

Backup decks, program listings with samples of the output (including plots) also have been provided. These programs are briefly identified below.

There are also numerous tape files containing absorption data as well as three current direct access files. A list identifying these tapes and files has been prepared for the user.

ABSPLT	Produces large-scale multiple plots for the absorption coefficients.
DA*	This file is made up of three FORTRAN elements, OPCODE, UPDATE, and PRNT. Each of these become independent data-handling programs when mapped into absolute elements with the subroutine DACCESS. Program OPCODE opens a 270 track (may be changed) FASTRAND file for the absorption coefficients ( $\text{cm}^{-1}$ ). This size file will contain about $36 \times 8500$ zeros. UPDATE allows absorption coefficients to be read from magnetic tape or FASTRAND files into the desired location in the opened direct access file. PRNT will print out all, or any desired portion, of this file.
DEN	Small routine to select and format ASA density data for the JVALUE program.
JONE3	Program to average absorption data over 1 Å intervals. Generally, a two-point interpolation is used for structured data and a four-point interpolation for smooth data. It is necessary to check the integrity of the maxima and minima for any except linear interpolation since these may be offset. ABSPLT allows plotting of the generated and original data on one grid. This program has an internal plot routine (subroutines QA and QB); however, the since-acquired COMPLIT software is superior for purposes of comparison.
JVALU5	Uses pre-calculated solar flux values to calculate photodissociation rates for species not included in ASA such as those important to the Freon problem.
DENPLT/ DNPLT	Generates density profiles from ASA output or from JVALUE data.

FLUX        Program which converts solar flux intensities from units of watts  $\text{m}^{-2}\text{nm}^{-2}$  to the average number of photons- $\text{cm}^{-2}\text{\AA}^{-1}\text{sec}^{-1}$ .

FMT        Blocks multiple sets of photodissociation rates for comparison.

JAYPLT/  
JYPLT2     Plotter for the individual photodissociation rates and for multiple plotting of photodissociation rates for purposes of comparison.

LEEPLT     Individual plots of absorption coefficients with variable grid size used to compare generated data with original values.

MEAN       Uses multiple FASTRAND files of photodissociation rates to calculate mean rates.

RADPLT     Program to generate large scale plots (500  $\text{\AA}$  intervals) of the solar flux output from JVALUE.

SOLPLT     Special purpose, small scale plotting routine for the altitude dependent solar flux generated by JVALUE. Experimental data points may be plotted with the line plot in version 4.

ZENITH     JVALUE subroutine, modified upon request to run as an independent program, which allows the calculation of up to 50 zenith angles at a time.

\*I wish to express my appreciation to Walter Decker, formerly stationed at White Sands Missile Range, for developing these programs.

I also wish to express my gratitude to Mr. Robert Lee, who recently retired from ASL, for his extensive help in programming over the past several years.